Student Name: _		
Student Number:		

GE 213.3 - Mechanics of Materials

MIDTERM EXAMINATION

March 2, 2005

Professor: B. Sparling Time Allowed: 3 Hours

• Closed book examination; Calculators may be used

• The value of each question is provided along the left margin

• Supplemental material is provided at the end of the exam (formulas)

• Show all your work, including all formulas, calculations and units

• Write your work in the space provided on the examination sheet. (The backs of the examination sheets may also be used if required)

Quest. 1:_____

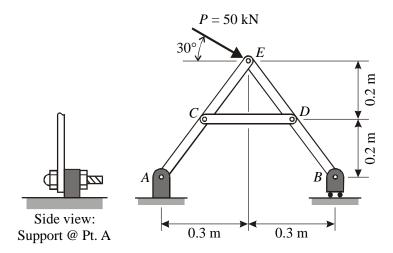
Quest. 2:_____

Quest. 3:_____

Quest. 4:_____

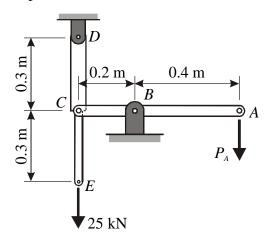
MARKS

- 25 QUESTION 1: The three member assembly shown below has a pinned support at Point A and a roller support at Point B. An inclined force, P = 50 kN, is applied at Point E. All connections in the assembly are pinned connections.
 - a) If the pin at Point A has a diameter of 25 mm and is fabricated from a material with an ultimate shear strength of $t_U = 180 \text{ MPa}$, determine the factor of safety for that pin.
 - b) If the central portion of member CD (i.e. away from the pins at either end) has a square cross-section and is fabricated from a material with an allowable normal stress of $\mathbf{s}_{all} = 150 \text{ MPa}$, determine the required cross-sectional dimensions for the central portion of member CD.

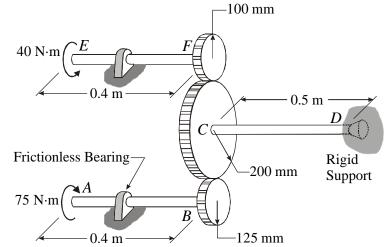


QUESTION 2: Rigid bar ABC is supported at Point B and connected to the vertical stepped bar DCE at Point C. All connections are pinned connections. Stepped bar DCE is continuous from Point D to Point E and is fabricated from material with an elastic modulus of E = 150,000 MPa and has a cross-sectional area of 500 mm² from Points D to C, and a cross-sectional area of 200 mm² from Points C to E.

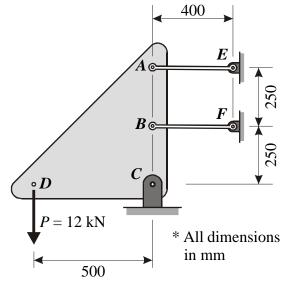
If a vertical force of 25 kN is applied at Point E as shown, determine the magnitude of the vertical force P_A applied at Point A so that the vertical displacement of Point E will be zero.



- 25 **QUESTION 3:** Three solid shafts (AB, CD and EF), each of which has a diameter of 30 mm, are connected by three gears of different sizes, as shown below. End D of shaft CD is rigidly attached to a support that prevents rotation. External torques are applied at the free ends A and E. The shafts are fabricated from a material with a modulus of rigidity G = 77,000 MPa.
 - **a)** Determine the maximum shear stress in shaft *CD*.
 - **b)** Calculate the magnitude and direction of the angle of twist at Point *E*.



- QUESTION 4: Rigid triangular plate ABCD has a pinned support at Point C and is connected to two horizontal rods AE and BF that have pinned connections at both ends. The rods have a cross-sectional area of 50 mm^2 , an elastic modulus of E = 125 GPa, and a coefficient of thermal expansion of $\mathbf{a} = 23 \times 10^{-6} / {}^{\circ}C$; they are unstressed prior to the application of the vertical load P = 12 kN at Point D. If, after the application of load P, the temperature of both rods is decreased by 20° C, determine:
 - a) The axial force in Rod AE; and
 - **b**) The horizontal displacement at Point *A*.



Supplemental Material:

- Static Equilibrium: $\Sigma F_x = 0$; $\Sigma F_y = 0$; $\Sigma F_z = 0$ & $\Sigma M_x = 0$; $\Sigma M_y = 0$; $\Sigma M_z = 0$
- Normal Stress: $\mathbf{s}_{avg} = \frac{P}{A}$ $F = \int_{A} \mathbf{s} \, dA$
- **Direct Shear Stress:** $t_{avg} = \frac{V}{A}$ (Single) or $t_{avg} = \frac{V}{2A}$ (Double)
- Bearing Stress: $s_b = \frac{P}{t d}$
- Allowable Stress: $F.S. = \frac{P_U}{P_D}$ or $F.S. = \frac{S_U}{S_D}$; $S_{all} = \frac{S_U}{F.S.}$ $P_{all} = S_{all}$ A $A_{req} = \frac{P_D}{S_{all}}$
- Stresses on Oblique Planes: $\mathbf{S}_{q} = \frac{P \cos \mathbf{q}}{A_{o}/\cos \mathbf{q}} = \frac{P}{A_{o}} \cos^{2} \mathbf{q}$; $\mathbf{t}_{q} = \frac{P \sin \mathbf{q}}{A_{o}/\cos \mathbf{q}} = \frac{P}{A_{o}} \sin \mathbf{q} \cos \mathbf{q}$
- Average Normal Strain: $e = \frac{d}{L_o} = \frac{L^* L}{L}$
- Hooke's Law: s = E e
- Axial Deformations: $d = \frac{P L_o}{A_o E}$; $d_{tot} = \sum_i \frac{P_i L_i}{A_i E_i}$; $d = \int_0^L \frac{P(x)}{A(x) E(x)} dx$
- Thermal Deformations: $d_T = a (\Delta T) L_o$ $e_T = \frac{d_T}{L_o}$
- Poisson's Ratio: $\mathbf{e}_y = \mathbf{e}_z = -\mathbf{n} \ \mathbf{e}_x$ $\mathbf{e}_y = \mathbf{e}_z = -\frac{\mathbf{n} \ \mathbf{s}_x}{E}$
- General Hooke's Law: $\mathbf{e}_x = \frac{\mathbf{S}_x}{E} \mathbf{n} \frac{\mathbf{S}_y}{E} \mathbf{n} \frac{\mathbf{S}_z}{E}$; $\mathbf{e}_y = -\mathbf{n} \frac{\mathbf{S}_x}{E} + \frac{\mathbf{S}_y}{E} \mathbf{n} \frac{\mathbf{S}_z}{E}$; $\mathbf{e}_z = -\mathbf{n} \frac{\mathbf{S}_x}{E} \mathbf{n} \frac{\mathbf{S}_y}{E} + \frac{\mathbf{S}_z}{E}$
- Shearing Strain & Stress: $q^* = \frac{p}{2} g_{xy}$; $g_{xy} = \frac{t_{xy}}{G}$; $g_{yz} = \frac{t_{yz}}{G}$; $g_{zx} = \frac{t_{zx}}{G}$; $G = \frac{E}{2(1+n)}$
- Resultant Torque: $T = \int_A r t \, dA$
- Torsional Strains: $g = \frac{r f}{L}$ $g_{\text{max}} = \frac{c f}{L}$ $g = \left(\frac{r}{c}\right) g_{\text{max}}$
- Torsional Stresses: $t = \left(\frac{\mathbf{r}}{c}\right)t_{\text{max}}$ $t_{\text{max}} = \frac{T c}{J}$ $t = \frac{T \mathbf{r}}{J}$ $J = \int_{A} \mathbf{r}^2 dA = \frac{\mathbf{p}}{2} c^4$
- Torsional Angle of Twist: $f = \frac{T L}{J G}$
- Torsion Gear Compatibility: $\phi_1 \rho_1 = \phi_1 \rho_2$
- Pure Bending Normal Strain: $\mathbf{e}_x = -\frac{y}{r}$ $\mathbf{e}_{max} = c/r$ $\mathbf{e}_x = -\frac{y}{c} \mathbf{e}_m$
- Pure Bending Normal Stress: $\mathbf{s}_x = -\frac{y}{c}\mathbf{s}_m$ $\mathbf{s}_x(y) = -\frac{My}{I}$ $\mathbf{s}_{\text{max}} = \frac{Mc}{I}$
- **Bending Section Properties:** $I = \int_A y^2 dA$; Centroid: $\int_A y dA = 0$
- Properties of Composite Areas: $\overline{y} A = \sum_{i} y_i A_i$ $I = \sum_{i} (I_i + A_i d_i^2)$